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Microstrip photon counting device for single x-ray counting

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**Description**

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**Microstrip photon counting device for single x-ray counting**

The invention relates to a photon-counting imaging device for single x-ray counting.

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X-ray diffraction patterns are useful in the analysis of molecular structures, such as protein and virus molecules, and require photon counting imaging devices. Especially, protein and virus crystallography imposes stringent requirements on x-ray detectors, particularly where the x-ray source is high flux synchrotron radiation that enables an experiment to be done rapidly. Furthermore, an important and developing field is time-resolved diffraction experiments using synchrotron radiation, such as crystallography and/or powder diffraction analysis. Monitoring a time-dependent reaction in a sample, i.e. a crystal or a powder, can elucidate the time-dependent crystal/molecular changes that occur in a chemical reaction as well. High time resolution speed is often critical in such monitoring.

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In the literature, a high speed crystallography detector is disclosed by the US patent 5,629,524 and a solid-state image sensor with focal-plane digital photon-counting pixel array is disclosed by the US patent 5,665,959. The latter patent describes and illustrates a focal-plane array comprising an array of NxN photodetector diodes connected to a digital photon-counting means for ultralow level image light detection and digital image pixel readout means for each pixel comprising separate CMOS buffer amplifiers that exhibit the following characteristics: low power ( $< 1 \mu\text{W}$  per pixel average), high photoelectron charge to voltage conversion gain ( $\approx 1 \text{ mV/e}^-$ ), low noise ( $< 1 \text{ e}^-$ ), small cell pitch ( $< 30$

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$\mu\text{m}$ ), easy scalability (to 10  $\mu\text{m}$ ), self biasing capability, sufficient gain uniformity ( $\sim 10\%$ ) for multiple event discrimination, and bias current programmability. Any incident photon during the sampling period generates a photoelectron at the output of the detector diode connected to the input of the amplifier. That photoelectron changes the potential of the buffer amplifier's input capacitance. This change in potential causes the high-gain buffer amplifier to present a sufficiently large voltage change at the output of the amplifier to be above the system noise level.

The drawback of this disclosure remains substantially in the design of this photon counting device that is dedicated to detect with brilliant sensitivity a single photon having its energy in the range of the visible light (several eV). This device can therefore be used for infra-red binoculars or for space-based telescopes and spectrometers. The electronic circuitry is therefore that sensitive that an incident photon is amplified in order to saturate the buffer of the amplifier. An additional incident photon occurring in the same photodetector diode within the same sampling period as the first incident photon therefore can not be detected unless the buffer is reset. This photon detecting device is therefore completely useless for the above-mentioned purposes of x-ray photon detection.

Nevertheless, the general design of the semiconductor chip is preferably a hybrid using a separate semiconductor material for two chips selected to be optimum for the photovoltaic type of detector diodes in one and the buffer amplifier and multiplexing circuit in the other chip bump bonded to the first to make connections between the output interface of the detector diodes on one chip and the input interface of the buffer amplifier on the other chip with the photodetector diodes buffer amplifier in one semiconductor chip and the multiplexing means and digital counters on the second semiconductor chip bump bonded to the first. As disclosed in

the US patent 5,629,524 a suitable material for the electrical bump connection is Indium. But even this device for x-ray photon detection can not be used in high dynamic investigation since the electronic circuitry is limited due to the switching dead time that is required to integrate the charge of the photo electrons subsequently to a chain of capacitors (referred to as a M-bit shift register) which have to be read out afterwards serially due to its chain-like arrangement. It could be easily understood that the performance of this circuitry is limited to its switching intervals for charging and scanning the capacitors.

Another prior art document worth to be mentioned is the US patent No. 5,812,191 disclosing a semiconductor high-energy radiation imaging device having an array of pixel cells including a semiconductor detector substrate and a semiconductor readout substrate. The semiconductor detector substrate includes an array of pixel detector cells, each of which directly generates charge in response to incident high-energy radiation. The semiconductor readout substrate includes an array of individually addressable pixel circuits, each of which is connected to a corresponding pixel detector cell to form a pixel cell. Each pixel circuit includes charge accumulation circuitry for accumulating charge directly resulting from high-energy radiation incident on a corresponding pixel detector cell, readout circuitry for reading the accumulated charge, and reset circuitry for resetting the charge accumulation circuitry. Unfortunately, the accumulated charge is stored as analog data using a circuitry having two transistors, one transistor acting as the charge store while the other acts as a readout switch responsive to an enable signal. This design restricts the circuitry to allow individual addressing each pixel but only discharge the accumulated analog charge to an output line when activated by its respective enable signal. This circuitry does not enable any further manipulation of the pixel detector cells.

Another imaging device for imaging radiation according to the international patent application WO 98/16853 includes an image cell array. The image cell array includes an array of  
5 detectors cells which generates charge in response to instant radiation and an array of image cell circuits. Each image cell circuit is associated with a respective detector cell. The image cell circuit includes counting circuitry for counting plural radiation hits incident on an associated  
10 detector cell. Preferably, the image cell circuit includes threshold circuitry connected to receive signals generated in the associated detector cell and having values dependent on the incident radiation energy. The counting circuitry is then connected to the threshold circuitry for counting only  
15 radiation hits within a predetermined energy range or ranges. The electronic readout circuitry is designed to comprise a loadable shift register storing the data serially in a row that means the input data is the data from the previous pixel and the output delivers the actual data to the next pixel.  
20 The main drawback of this arrangement consists in the susceptibility to a failure of a complete row of the detector array if only one the readout circuitry in a row fails.

Furthermore, using x-ray diffraction for the analysis of the  
25 crystallographic structure of a sample a fast and reliable measurement procedure requires a comparably large detector array for covering a sufficient large spatial area. It is apparent from the required electronic equipment that an increasing number of detector arrays is followed by an  
30 increasing number of electronic equipment and/or a prolonged evaluation procedure.

Resuming the prior art document it will be apparent that none of the document disclose a photon counting imaging device  
35 that allow high readout performance und superior reliability of operation having a very fast and immediate control for the readout electronics and the photodetector diodes.

Therefore, it is the aim of the invention to increase the performance and the reliability of a complete photon-counting imaging device.

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This aim is achieved according to the invention by a photon-counting imaging device for single x-ray counting comprising:

- a) a layer of photosensitive material;
- b) a source of bias potential;
- 10 c) a source of threshold voltage supply;
- d) an NxM array of photodetector diodes arranged in said layer of photosensitive material; each of said photodetector diodes having a bias potential interface and a diode output interface, said bias potential interface of each photodetector diode being connected to  
15 said bias potential;
- e) an NxM array of high gain, low noise readout unit cells, one readout unit cell for each photodetector diode being controlled by a data processing means; and
- 20 f) the array of photodetector diodes is designed as a microstrip detector having  $N=1$  columns and  $M>1$ , preferably  $10 < M < 10^5$ , rows.

25 This photon counting imaging device allows a very fast and efficient readout procedure and facilitates to arrange a larger number of photo-detector diodes orientated vertically in length to build a convex array of x-ray detection diodes. With a stable x-ray beam, i.e. taken from a synchrotron, and the feasibility of turning the sample stepwise, the complete  
30 crystalline structure of the sample can be investigated in a comparably short time.

The dimension are in an advantageous way chosen to comprise said rows having a width of about 5 to 50  $\mu\text{m}$ , preferably  
35 about 10 to 20  $\mu\text{m}$ , a length of about 0.5 to 50 mm, preferably 5 to 10 mm, and a pitch of 10 to 100  $\mu\text{m}$ , preferably 25 to 75  $\mu\text{m}$ .

A proper design of the readout unit cell provides a readout unit cell having an input interface connected to said diode output interface, a high-gain voltage amplifying means  
5 comprising a comparator unit, a digital counter unit, comprising a digital counter, and a digital counter output interface connected in series, each digital counter unit counting an output signal of the comparator unit; said output signal is proportional to a number of electron hole pairs  
10 generated by a photon in the respective photodetector diode.

In order to globally or individually adjust a proper sensisitivity of all or only of an individual detector diode said source of threshold voltage supply to said high-gain  
15 voltage amplifying means comprises an adjustable source of threshold voltage correction supply, both being controlled by the data processing means via the multiplexer means.

In order to increase the position resolution of an incident  
20 photon the data processing means may provide means for enhancing the position resolution of an incident photon; said means for enhancing the position resolution comprising a comparator means comparing the signals of two adjacent photodetector diodes. By the comparison of the signal from  
25 the two adjacent photodetector diode a photon can be assigned to an virtual intermediate photodetector diode in case the charge of the electron hole pairs generated in the twilight zone between two adjacent photodetector diodes can be  
30 observed in partially in two adjacent photodetector diodes.

In order to take advantage of the afore-mentioned feature with respect to avoiding double counting the data processing means allow to determine an average amplitude for the gain of the electron hole pairs generated by an incident photon and  
35 to set a threshold voltage corresponding to less than half of the average amplitude; said data processing means evaluate coincident output signals in adjacent readout unit cells in



order to disable the counting in the adjacent readout unit cells having coincidentally delivered the lower output signal(s).

- 5 Another innovative feature with respect to the resolution of the device may provide the data processing means allowing to determine an average amplitude for the gain of the electron hole pairs generated by an incident x-ray photon and to set a threshold voltage corresponding to less than half of the
- 10 average amplitude; the data processing means may generate a virtual intermediate photodetector diode between two adjacent photodetector diodes; and an incident photon is assigned to said virtual intermediate photodetector diode in case the output signals in two readout unit cells assigned to adjacent
- 15 photodetector diodes exceed said threshold voltage ( $V_{\text{Thresh}}$ ) coincidentally.

A consequential measure provides the data processing means to control via the multiplexing means one or more of the

20 following issues:

- a) programming of the readout unit cell via a port;
  - b) readout of the data in the readout unit cell via a port;
  - c) calibration of the readout unit cell, preferably the
  - 25 high gain voltage amplifier means, via a port; and
  - d) analyzing the analog signal in the high gain voltage amplifier means for the purpose of diagnosis via a port.
- 30 This measure now in detail explains the advantages derivable from the afore-mentioned multiplexing means that allow the direct access to each readout unit cell. The calibration in the regard is considered to be able to calibrate the bias of each photodetector diode. Another calibration can be achieve
- 35 by the afore-mentioned adjustment of the threshold voltage by the threshold voltage correction supply. For evaluating the status of the photodetector diode and/or the analog part of

the readout unit cell circuitry in detail the analysis of the analog signal processed with the high gain voltage amplifier means is very helpful and could only be achieved by the ability to address a distinct detector pixel using two independent shift registers of the multiplexing means.

For constructing a photon-counting imaging device detecting the photon radiation over a comparably large focal or flat area a suitable architecture can provide said NxM array of photodetector diodes, said NxM array of said readout unit cells being arranged on a first substantially flat support plate for building a sensor module, and a sensor module control board being arranged on a second substantially flat support plate; said first substantially flat support plate and said second substantially flat support plate being arranged under an angle to each other. A suitable angle may reside within a range of 20 to 180°, preferably 45 to 100°. This measure allows to construct a plane or curved detector surface area made from a number of sensor modules having stretched out on the opposite side of its detector surface the sensor module control board comprising at least partial the required readout electronic equipment, i.e. the data processing means or at least part of them.

For forming a large solid-state photon-counting imaging device a number of the afore-mentioned sensor modules being arranged in a substantially flat or curved VxW array wherein V and W are integer numbers at least one of them larger than one.

Examples of the invention are described below in accordance with the drawings which depict:

Figure 1 a schematic view of a photodetector diode;

Figure 2 a schematic view of a part of a sensor module comprising an array of photodetector diodes as one shown in Figure 1;

5 Figure 3 a schematic view of a microstrip detector;

Figure 4 a schematic view of the readout electronic of a readout unit cell assigned to and connected with a photodetector diode as shown in Figur 1;

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Figure 5 a sensor module as a basic element for a photon-counting imaging device having a number of those sensor modules with a sensor module control board;

15 Figure 6 a schematic view on a sensor module readout chip;

Figure 7 a schematic view on photons entering the microstrip detector according to figure 3; and

20 Figure 8 a schematic view of the signals caused by the photons as shown in figure 7 entering the microstrip detector.

25 Figures 1 illustrates schematically the architecture of a photodetector diode 2 having a doped semiconductor  $p^+$ ,  $n^+$ ,  $n^{++}$  trespassing section 4. The material choosen for the photodetector diode 2 depends on the desired bandgap energy required to generate an electron hole pair by the photo-effect. Suitable materials are undoped amorphous silicon having band gap of 1.12 eV and a bundle of IV-IV compounds and III-V compounds (indium and gallium salts, like gallium arsenide or indium antimonide).

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A incident photon 6 having an energy in the range of several  
35 KeV before entering the doped semiconductor  $p^+$ ,  $n^+$ ,  $n^{++}$  trespassing section 4 passes through an aluminium cover layer 8 and causes according to its energy and to the energy gap of

the doped semiconductor  $p^+$ ,  $n^+$ ,  $n^{++}$  trespassing section a respective number of electron hole pairs 10 under x-ray annihilation. In the drawing this number of electron hole pairs is exemplarily shown by one electron-hole pair 10 being  
5 divided by the voltage generated by a source of bias potential 12. The evaluation of the charge occurred from the electron hole pairs 10 will be described below with reference to figure 4.

10 Figure 2 shows a schematical view of a two-dimensional pixel detector 14 having a number of photodetector diodes 2 arranged in an array of 22 rows and 32 columns (compare figure 6). The photodetector diodes 2 have a length  $l$  and a  
15 width  $w$  of about 200  $\mu\text{m}$  and a height of about 300  $\mu\text{m}$ . Below the plane of these photodetector diodes 2 a readout chip 16 having a corresponding number of readout unit cells 18 is arranged for collecting the charge from the electron hole pairs 10 generated in the respective photodetector diodes 2. The electrical conjunction between a diode output interface  
20 20 of the photodetector diodes 2 and an input interface 22 of the readout unit cells 18 is achieved by bump bonding using indium bumps 24.

Figure 3 depicts a schematical view of a microstrip detector  
25 26 having on a hybrid support 28 arranged a number of thirty-eight strip-type photodetector diodes 30 build in a microstrip sensor sector 32 of the hybrid support 28. The strip-type photodetector diodes 30 have a width of about 15  $\mu\text{m}$ , a length of about 8 mm and a pitch of about 50  $\mu\text{m}$ . Next  
30 to the microstrip sensor sector 32 a microstrip readout sector 34 is arranged having a number of readout unit cell 36 (not shown in detail, described below) corresponding to the number of strip-type photodetector diodes 30. These readout unit cells 36 are connected with their input interface 22 to  
35 the photodetector diodes 30 by bond pads 38 which additionally connect an output interface 40 of the readout

unit cells 36 to a digital counting sector 42 which is described below, too.

Figur 4 now depict a schematic view of a electronic readout equipment 44 as it can be used for both the two-dimensional pixel detector 14 and the microstrip detector 26. The electronic readout equipment 44 is divided into an analog block 46 and a digital block 48. The analog block 46 starts with the bump pad 22 (interface), 38 resp. connected to an input terminal of a charge sensitive amplifier Amp. For calibration purposes a source for calibration voltage  $U_{cal}$  is connected via a capacitor C to the input terminal of the CS amplifier Amp, too. The capacity of the capacitor has been chosen to a comparably tiny capacity of about only 1.7 fF allowing to be sensitive enough that the photo-electrons can change the voltage over the capacitor C to an extend that this difference can be significantly amplified by the CS amplifier Amp hereinafter referred to as first output voltage signal.

This first output voltage signal is led to one of the two input terminals of a comparator amplifier CA which is additionally connected to a source of a threshold voltage supply  $U_T$ . The other input terminal of the comparator amplifier CA is additionally connected to a source of threshold voltage correction supply TC. This source of threshold voltage correction supply TC allows to bias the input terminals of the comparator amplifier CA. According to the predetermined bias of the input terminals of the comparator amplifier CA even the first output voltage signal from the CS amplifier Amp representing only a fractional part of the charge of the generated photo-electron hole pairs can be further processed and is therefore not suppressed during the later data processing and evaluating. This electronic readout equipment 44 enables the detection of fractions of the full charge of a the photo-electron hole pairs 10 generated by an incident x-ray what may occur when the photo-

electron hole pairs 10 are generated in the twilight zone located between two adjacent photodetector diodes 2.

As an example, the source of threshold voltage correction supply TC can be adjusted up to a level defined by one half of the full charge of the photo-electron hole pairs 10 generated in total by one x-ray photon. Consequentially, the distribution of the charge of the photo-electrons to adjacent photodetector diodes 2 can be further processed. A downstream data processing unit is now enabled to perform a differential evaluation of the digital output voltage signals of the comparators having its origin from the photo-electrons in adjacent photodetector diodes 2, whereby these photo-electrons have been generated by the same x-ray photon.

Downstream to the analog block 46 is the digital block 48 having generally the task to convert the digital output voltage signal into a digital counter signal that can be evaluated by multiplexing means MM provided with the data processing means DPM. Together with a enable/disable switch E/D different clock means, i.e. an external clock RCLK from the data processing means DPM control a clock generator CG for a digital counter unit SRC which itself is connected to a readout bus output RBO. The digital data stored in the digital block 48 of a distinct readout unit cell can then be readout if a row select RS and column select CS are set high to set high an AND-gate &.

Figure 5 illustrates a solid-state photon-counting imaging device 50 detecting the photon radiation over a comparably large flat area. The present architecture combine a number of sixteen pixel sensors 14 being arranged on a first substantially flat support plate 52 for building a sensor module 54, and a sensor module control board 56 being arranged on a second substantially flat support plate 58 hosting the electronic evaluation equipment, i.e. multiplexing means MM, data processing means DPM, which

follow the afore-mentioned electronic readout equipment 44. The first substantially flat support plate 52 and the second substantially flat support plate 58 being arranged under an angle of 90°. This measure allows to construct a plane or  
5 curved detector surface area (here not shown in the drawings) made from a number of sensor modules 54 having stretched out on the opposite side of its detector surface the sensor module control boards 56.

- 10 Figure 6 now shows a schematic view on a sensor module readout process indicating that appropriate multiplexing means MM allowing with a row select logic SR and a column select logic CR to address a predetermined readout unit cell 18 in order to readout the value of the digital counter SRC.  
15 This addressability lead to the capability of the complete photon-counting imaging device 50 to access and/or control continuously or temporarily each readout unit cell. The photon-counting imaging device 50 owns the capability to access and/or control via the data processing means DPM via  
20 the multiplexing means MM one or more of the following issues:
- a) programming of the readout unit cell via a port DIN;
  - b) readout of the data in the readout unit cell via a port DOUT;
  - 25 c) calibration of the readout unit cell, preferably the high gain voltage amplifier means 46, via a port CAL; and
  - d) analyzing the analog signal in the high gain voltage amplifier means 46 for the purpose of diagnosis via a  
30 port AOUT.

All the afore-mentioned ports DIN, DOUT, CAL and AOUT are comprised in the readout bus RB that is controlled by the data processing means DPM. With respect to the multiplexer  
35 means MM, it has to be pointed out additionally that this multiplexer means MM is substantially a separate chip being located on the sensor module control board 56. This separate

chip generates a chip select for at least one or all of the readout chips assigned to each of the pixel sensors 14. Each readout chip itself comprises a column select shift register and a row select shift register for selecting a distinct  
5 sensor pixel. Therefore, in principal the multiplexing means MM are assigned to both each readout chip and the sensor module control board 56.

10 Figures 7 and 8 are now used to introduce the afore-mentioned concept of charge sharing in the microstrip detector 26 allowing the enhancement of the position resolution for the incident photon 6 entering into the doped semiconductor  $p^+$ ,  $n^+$ ,  $n^{++}$  trespassing section 4. Dotted lines shall indicate the electric field line of the bias potential 12 enabling to  
15 collect the photoelectrons at the cathode of the photodetector diode 2 as schematically shown in figure 7. Two of the photodetector diodes 30 and their respective readout unit cells 36 are hereinafter referred to as a first channel Ch1 and a second channel Ch2. In the drawings according to  
20 figure 8 the situation with respect to the potentials caused by the incident photons 6a, 6b and 6c is shown. The charge of the electron-hole pairs 10 generated by the photons 6b and 6c absorbed in the doped semiconductor  $p^+$ ,  $n^+$ ,  $n^{++}$  trespassing section 4 in an intermediate region 60 between the two  
25 channels Ch1 and Ch2 is divided between these two channels Ch1 and Ch2 according to the position of the photons 6b and 6c. The charge is shared to the two channels Ch1 and Ch2 and both channels Ch1 and Ch2 show an analogue pulse at the output of the charge sensitive amplifier Amp as it can be  
30 seen from figures 8b and 8c.

The pulses after the amplifier Amp (going into the comparator CA) for the photons 6a, 6b, 6c are shown in figure 8a, 8b and 8c resp. Depending on setting of a threshold voltage  $V_{Thresh}$  in  
35 the comparator CA, a certain risk occurs that the photons 6a, 6b and 6c are counted twice ( $V_{thresh} < A_{max}/2$ ) or not at all ( $V_{thresh} > A_{max}/2$ ). Both effects are highly undesirable and



double counting is a serious problem for diffraction experiments.

It is therefore advantageous to implement in the data  
5 processing means DPM a logic that prohibits double counting  
for low threshold voltages ( $V_{\text{thresh}} < A_{\text{max}}/2$ ). The logic to avoid  
double counting can easily be implemented using the fact that  
the output signal OS of the comparator CA for the pulse with  
10 the higher amplitude completely encloses the output signal of  
the comparator CA for the neighbouring channel with the lower  
amplitude as this can be seen in figure 8b. Figure 8b  
represents the distribution of the photoelectrons caused by  
the photon 6b that enters the intermediate region 60 a bit  
15 more on the side of the second channel Ch2. The pulse  
therefore generated in the second channel Ch2 exceeds the  
respective pulse in the first channel Ch1.

Therefore, the output signal OS of the comparator CA of the  
channel with the higher amplitude, here the second channel  
20 Ch2, can be used to disable the adjacent channel, here the  
first channel Ch1, showing the lower signal amplitude. Double  
counting is therefore avoided by disabling the weaker  
channel. I.e. using the output signal OS of the comparator CA  
of a dominating channel to disable the comparator CA via  
25 the Enable/Disable Switch E/D (or the counting) of its two  
neighbouring channels provided the coincidently occurring  
amplitude of the central channel is above the threshold.

The effect of the charge sharing over two adjacent channels  
30 can also be used advantageously to improve the position  
resolution above the position resolution given by the  
patterning of the photodetector diodes 30. For example, this  
can be done by introducing intermediate channels in the  
readout electronics which either have a special analogue part  
35 summing the analogue signals from the two neighbours for  
restoring the full charge of the electron hole pairs caused  
by photons entering the intermediate region, or by avoiding

completely the analogue part for the intermediate channel, to design a virtual intermediate channel that only counts in case both the comparators CA of both neighbours give a coincident pulse that reaches in total substantially the level of the full charge of a photon completely absorbed in one channel. In the case of analogue summing a scheme like the one given above can be used to avoid double counting.

In the latter case either additional logic has to be implemented to avoid counting of the neighbours or, even easier, since the intermediate channel only counts if both neighbours count, the counter value of the intermediate channel can just be subtracted from both neighbours. This can be done off line. For the enhancement of the resolution the threshold voltage  $V_{\text{Thresh}}$  has to be in the range  $0 < V_{\text{Thresh}} < A_{\text{max}}/2$ , preferably closer to  $A_{\text{max}}/2$  than to zero.

List of reference number

	2	Photodetector diode
	4	Doped semiconductor $p^+$ , $n^+$ , $n^{++}$ trespassing
5		section
	6	Photon
	6a, 6b, 6c	Photons
	8	Aluminium cover layer
	10	Electron hole pairs
10	12	Source of bias potential
	14	Pixel detector
	16	Readout chip
	18	Readout unit cells
	20	Diode output interface
15	22	Input interface
	24	Indium bumps
	26	Microstrip detector
	28	Hybrid support
	30	Strip-type photodetector diodes
20	32	Microstrip sensor sector
	34	Microstrip readout sector
	36	Readout unit cells
	38	Bond pads
	40	Output interface
25	42	Digital counter section
	44	Electronic readout equipment
	46	Analog block
	48	Digital block
	50	Solid-state photon-counting imaging device
30	52	First substantially flat support plate
	54	Sensor module
	56	Sensor module control board
	58	Second substantially flat support plate
	60	Intermediate region
35	$A_{max}$	Average amplitude
	Amp	Charge sensitive Amplifier
	C	Capacitor

	CA	Comparator amplifier
	CG	Clock generator
	Ch1, Ch2	First channel resp. second channel of two adjacent readout unit cells
5	CS	Column select
	E/D	Enable/Disenable Switch
	MM	Multiplexing Means
	OS	Output signal
	RB	Readout bus
10	Reset	Digital counter reset
	RS	Row select
	SRC	Digital counter unit
	t	Time
	TC	Source for threshold voltage correction supply
15	U <sub>Cal</sub>	Source for calibration voltage
	U <sub>T</sub>	Source for threshold voltage supply
	V <sub>Thresh</sub>	Threshold voltage

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## 5 Patent Claims

1. A photon-counting imaging device (26) for single x-ray counting comprising:

- a) a layer of photosensitive material (4);
- b) a source of bias potential (12);
- c) a source of threshold voltage supply ( $U_T$ );
- d) an  $N \times M$  array of photodetector diodes (30) arranged in said layer of photosensitive material (4); each of said photodetector diodes (30) having a bias potential interface and a diode output interface (20), said bias potential interface of each photodetector diode (30) being connected to said bias potential (12);
- e) an  $N \times M$  array of high gain, low noise readout unit cells (36), one readout unit cell (36) for each photodetector diode (30) being controlled by a data processing means (DPM); and
- f) the array of photodetector diodes (30) is designed as a microstrip detector (26) having  $N=1$  columns and  $M>1$ , preferably  $10 < M < 10^5$ , rows.

2. A photon counting imaging device (26) according to claim 1, characterized in that each readout unit cell (36) comprises an input interface (22) connected to said diode output interface (20), a high-gain voltage amplifying means (46) comprising a comparator unit (CA), a digital counter unit (48), comprising a digital counter (RSC), and a digital counter output interface (RB) connected in series, each digital counter unit (48) counting an output signal (OS) of the comparator unit (CA); said output signal (OS) is proportional to a number of electron hole pairs (10) generated by a photon (6) in the respective photodetector diode (30).

3. The photon-counting imaging device (26) according to claim 1 or 2, characterized in that said rows having a width of about 5 to 50  $\mu\text{m}$ , preferably about 10 to 20  $\mu\text{m}$ , a length of about 0.5 to 50 mm, preferably 5 to 10 mm, and a pitch of 10 to 100  $\mu\text{m}$ , preferably 25 to 75  $\mu\text{m}$ .

4. The photon-counting imaging device (26) according to any one of the preceding claims, characterized in that said source of threshold voltage supply ( $U_T$ ) to said high-gain voltage amplifying means (46) comprises an adjustable source of threshold voltage correction supply (TC), both being controlled by the data processing means (DPM).

5. The photon-counting imaging device (26) according to any one of the preceding claims, characterized in that the data processing means (DPM) provide means for enhancing the position resolution of an incident photon (6); said means for enhancing the position resolution comprising a comparator means comparing the signals of two adjacent photodetector diodes (30).

6. The photon-counting imaging device (26) according to claim 5, characterized in that the data processing means (DPM) allow to determine an average amplitude ( $A_{\text{max}}$ ) for the gain of the electron hole pairs (10) generated by an incident photon (6) and to set a threshold voltage ( $V_{\text{Thresh}}$ ) corresponding to less than half of the average amplitude ( $A_{\text{max}}$ ); said data processing means (DPM) evaluate coincident output signals (OS) in adjacent readout unit cells (36) in order to disable the counting in the adjacent readout unit cells (36) having delivered the lower output signals (OS).

7. The photon counting imaging device (26) according to claim 5, characterized in that

the data processing means (DPM) allow to determine an average amplitude ( $A_{\max}$ ) for the gain of the electron hole pairs (10) generated by an incident x-ray photon and to set a threshold voltage ( $V_{\text{Thresh}}$ ) corresponding to less than half of the average amplitude ( $A_{\max}$ ); the data processing means (DPM) generate a virtual intermediate photodetector diode between two adjacent photodetector diodes (30); and an incident photon (6) is assigned to said virtual intermediate photodetector diode in case the output signals (OS) in two readout unit cells (36) assigned to adjacent photodetector diodes (30) exceed said threshold voltage ( $V_{\text{Thresh}}$ ).

8. The photon-counting imaging device (26) according to any one of the preceding claims, characterized in that the data processing means (DPM) control one or more of the following issues:

- a) programming of the readout unit cell (36) via a port (DIN);
- b) readout of the data in the readout unit cell (36) via a port (DOUT);
- c) calibration of the readout unit cell (36), preferably the high gain voltage amplifier means (46), via a port (CAL); and
- d) analyzing the analog signal in the high gain voltage amplifier means (46) for the purpose of diagnosis via a port (AOUT).

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**Abstract**

5

It is the aim of the invention to increase the performance and the reliability of a complete photon-counting imaging device.

10 This aim is achieved according to the invention by a photon-counting imaging device for single x-ray counting comprising:

a) a layer of photosensitive material;

b) a source of bias potential;

c) a source of threshold voltage supply;

15 d) an NxM array of photodetector diodes arranged in said layer of photosensitive material; each of said photodetector diodes having a bias potential interface and a diode output interface, said bias potential interface of each photodetector diode being connected to  
20 said bias potential;

e) an NxM array of high gain, low noise readout unit cells, one readout unit cell for each photodetector diode being controlled by a data processing means; and

25 f) the array of photodetector diodes is designed as a microstrip detector having  $N=1$  columns and  $M>1$ , preferably  $10 < M < 10^5$ , rows.

30 This photon counting imaging device allow a very fast and efficient readout procedure and facilitates to arrange a larger number of photo-detector diodes orientated vertically in length to build a convex array of x-ray detection diodes. With a stable x-ray beam, i.e. taken from a synchrotron, and the feasibility of turning the sample stepwise, the complete crystalline structure of the sample can be investigated in a  
35 comparably short time.

Fig. 3



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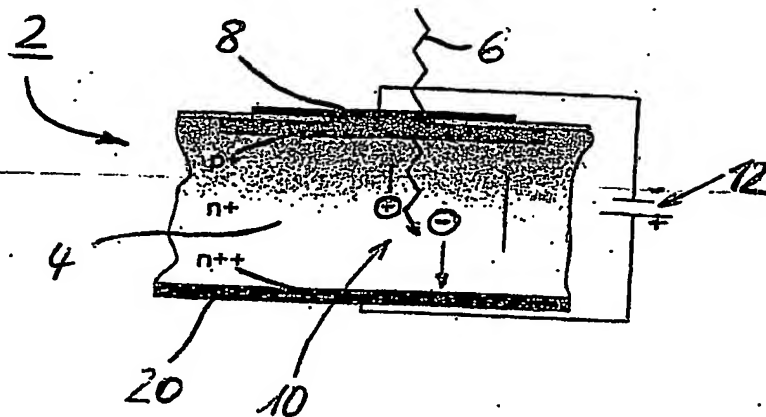


Fig. 1

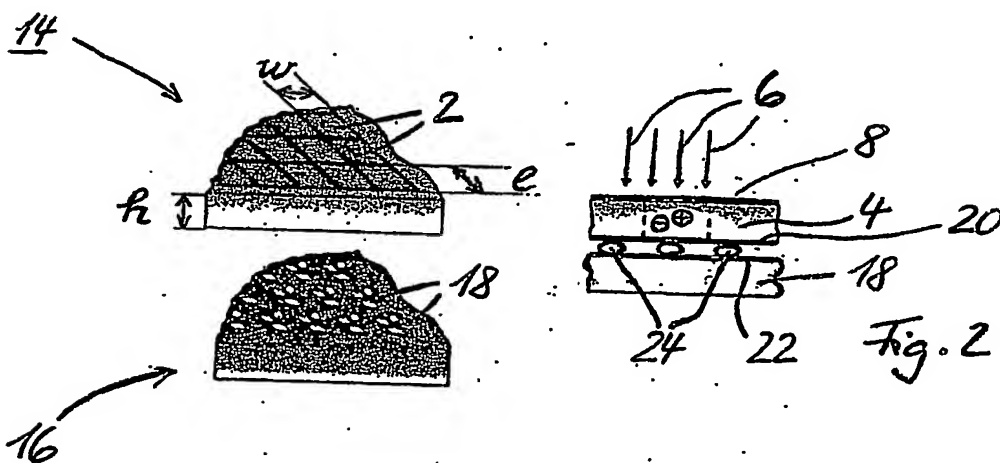


Fig. 2

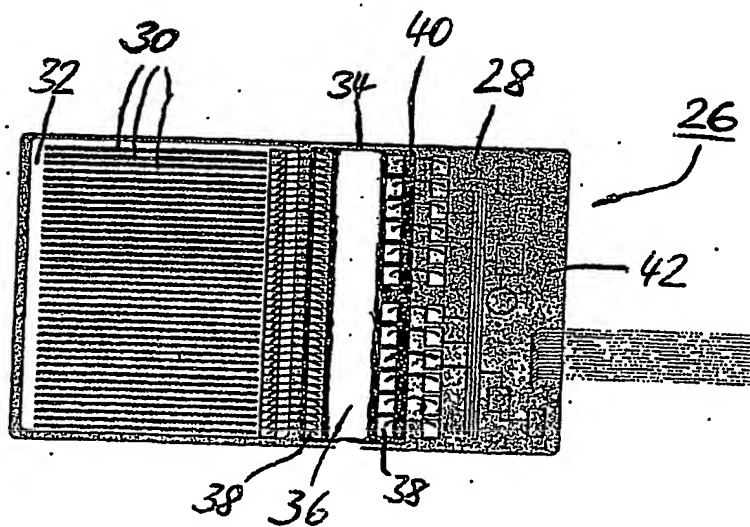
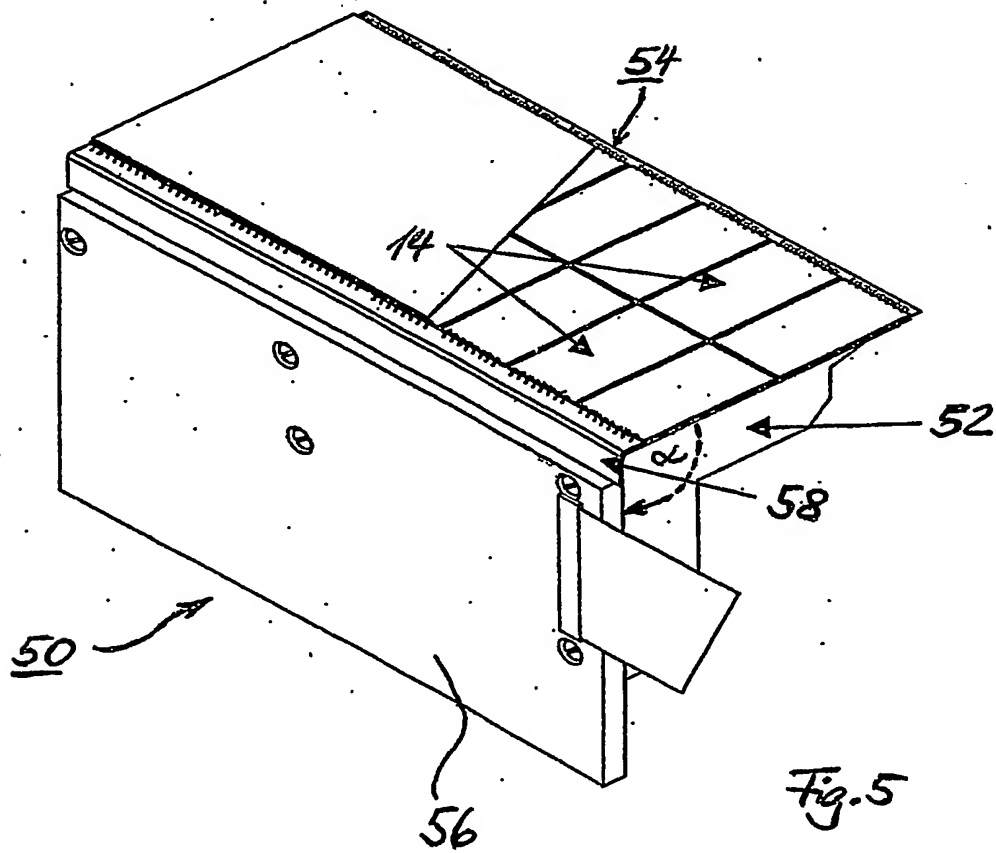
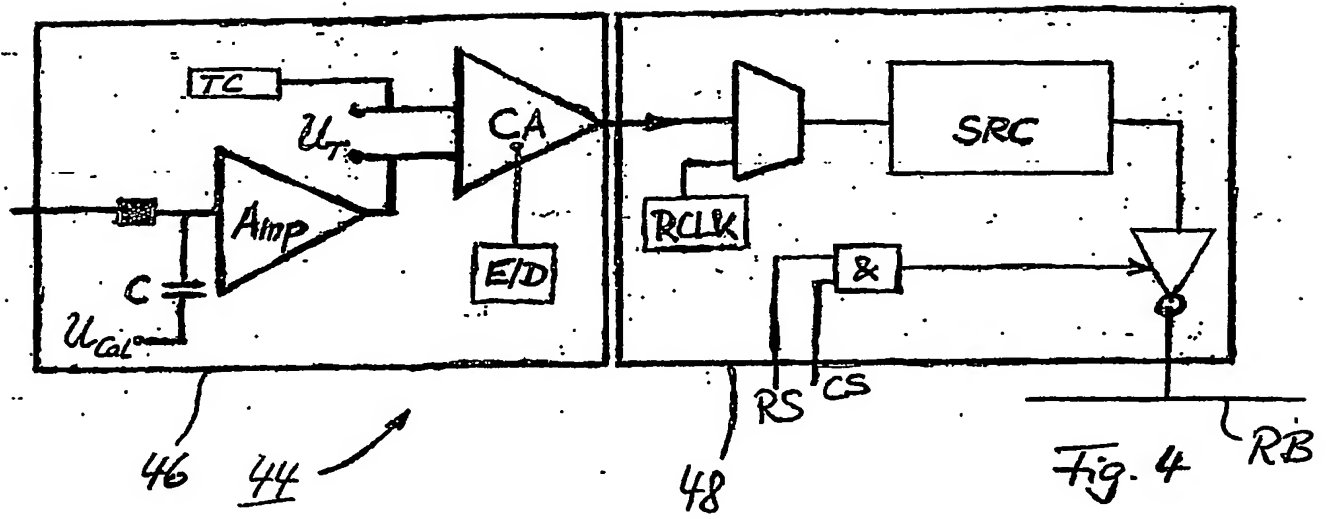
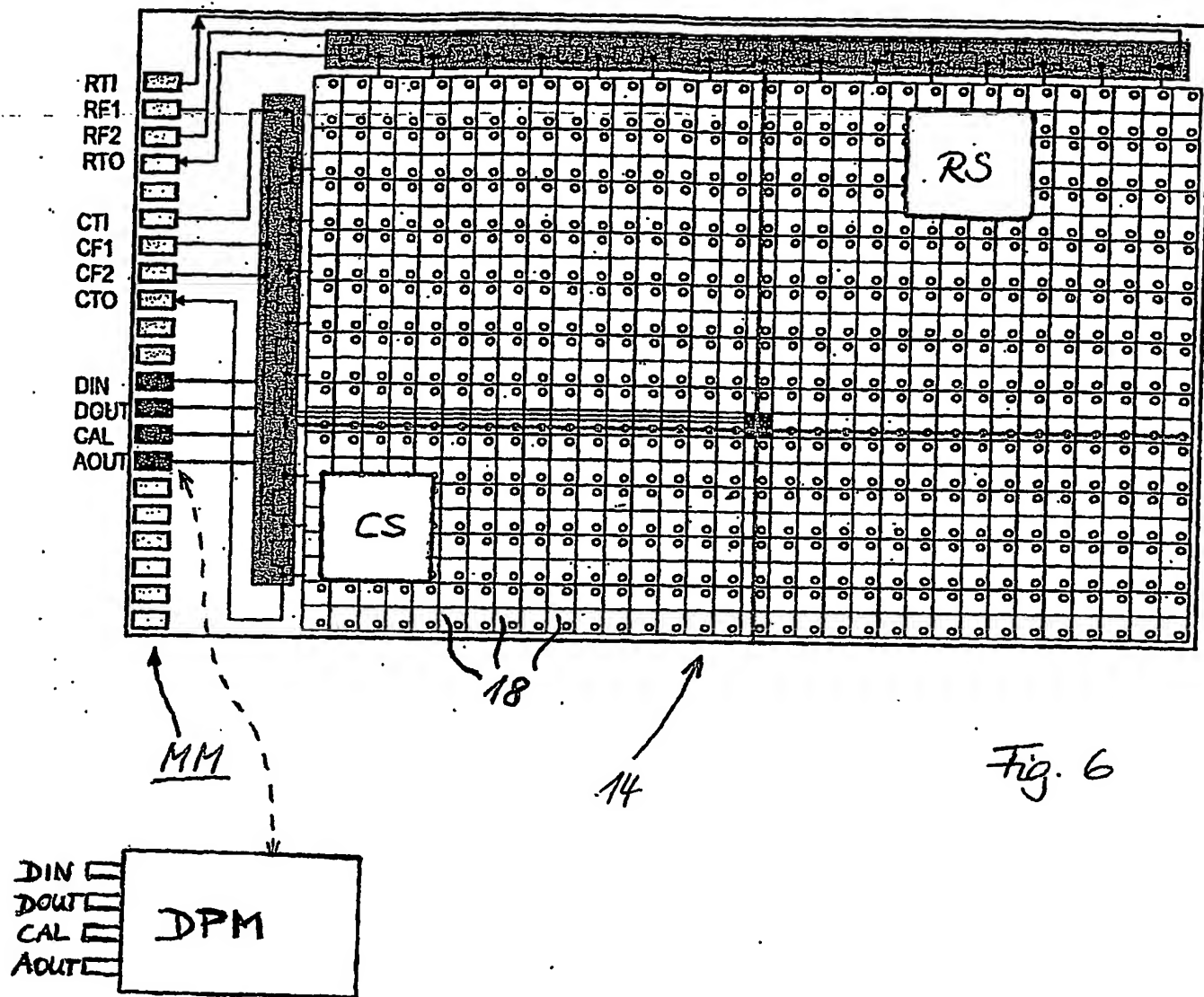


Fig. 3





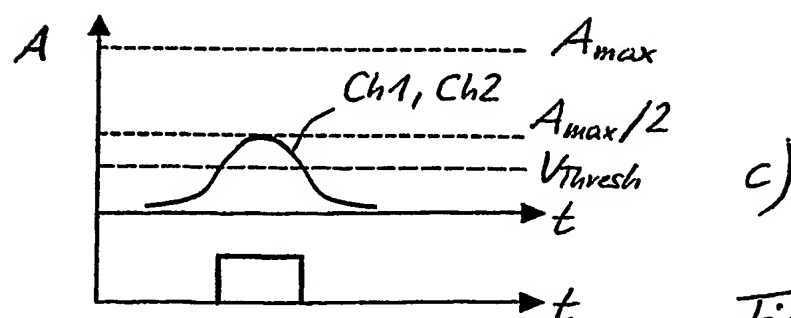
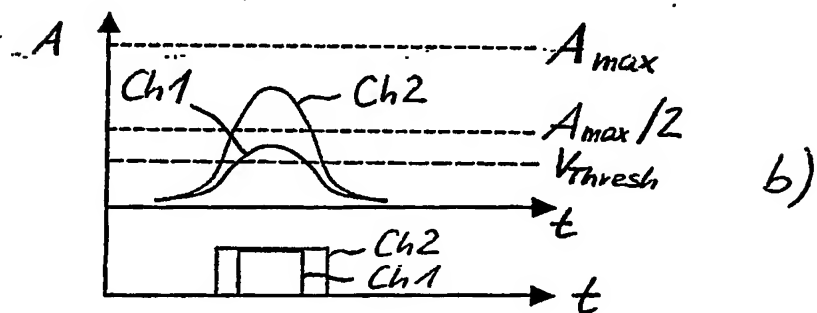
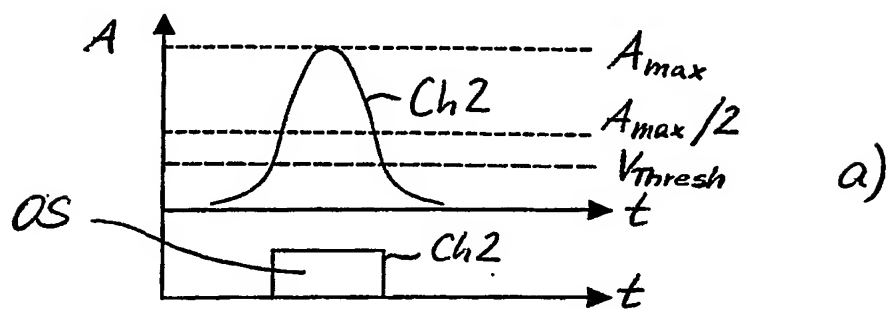
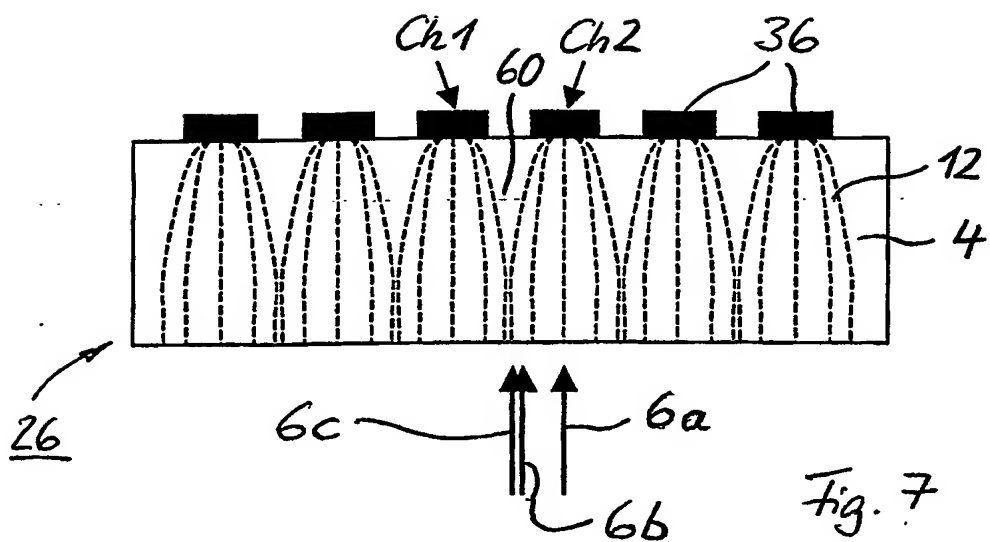


Fig. 8

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